

International NAFEMS Conference on Engineering Analysis, Modeling, Simulation and 3D-Printing (NAFEMS-3D) – 2016

Full paper

Simulation Driven Design Optimization for Reduction of Temperature on a High Current Density PCB

Nitesh Kumar Sardana, Susyamala Pavan Kumar Busam, Dr. Laxmidhar Biswal Robert Bosch Engineering and Business Solution Pvt. Ltd. Niteshkumar.sardana@in.bosch.com

Abstract

Market demand for lightweight and cost effective electronic products with multi-functional operations leads to the introduction of plastic housing and high current density on board. In general, automotive electronic products operate in harsh environment. With high current demand, Joule heating ($Q = I^2R$, where I is current and R is electrical resistance of trace/track) in copper tracks on board is highly pronounced. Managing heat dissipation both from components and tracks without cooling bank on housing is a thermal challenge.

For this study, the product consists of a plastic enclosure that houses printed circuit board (PCB) and electronic components that are capable of operation at higher current. The product consists of multiple inputs and outputs to support a variety of loads. The high current is distributed across multiple copper layers in PCB. These copper layers (due to the constraint in their size) experience high current density that leads to higher Joule heating. Apart from this, there are several heat dissipating components on board. As a result, the components are experiencing higher temperature. Electrical-Thermal simulation helps to (i) visualize the thermal field, (ii) identify bottlenecks to current flow, and (iii) identify hot spots in order to optimize the circuit layout for reducing the Joule heating.

In this study, Electrical-Thermal simulation is carried out using TRM. The model consists of lumped components with their respective power dissipation, thermal vias in PCB underneath the heat dissipating components, PCB base material (FR4), copper layers with discrete tracks for current flow and heat conduction, and electrical nets for current flow among copper layers, input-output pins and components. The effect of enclosure is manifested in the overall heat transfer coefficient that is applied on PCB and components as boundary condition. Overall heat transfer coefficient is derived from a system-level conjugate heat transfer model accounting for conduction, convection and radiation for the entire product. Electrical current (I) is assigned to input and out pins. Ambient temperature is applied to PCB and components as boundary condition.

Measurement at board-level is carried out in the lab via Thermal imaging and thermocouple measurements for thermal field and component temperature respectively. Simulation and measurement results are found to be within $\pm 3\%$.

After validating the simulation model, parametric study via simulation is carried out to optimize the copper tracks geometry and location of components and power dissipation of the components, PCB stack up and PCB base material properties. These parameters are evaluated against the cost of the product due to each change. This optimization helps in reducing the hot spots and temperature on the PCB, during the early development phase itself, and reduces the development cost as well as the product cost.

Keywords: Design Optimization, Electrical-Thermal Simulation, Joule heating, High Current Density, PCB

Introduction

With the rise in usage of electronics in automobile industry, the demand for light weight and cost effective electronics has increased exponentially in past few decades. Along with the packaging requirements, the functionality of electronics has increased, posing challenges for thermal management of electronics. To cater numerous functionalities required by the application, component density and current on Printed Circuit Board has increased too.

All these requirement has led to the introduction of plastic housing and high current density on board.

The amount of heat generated in copper tracks on board due to flow of current is

$$Q = I^2 R \tag{1}$$

Where,

Q: Joule heating, W

I: current flow in copper tracks on board, A

R: electrical resistance of copper tracks, Ω

Electrical resistance, R, is related to geometry and resistivity of the copper track:

$$R = \rho L/A \tag{2}$$

Where,

 ρ : Electrical resistivity of the copper track, $\Omega \cdot m$

L: length of the copper track, m

A: cross section of the track carrying current, m²

With increase in current, Joule heating poses bigger thermal challenges. The thermal challenges are amplified if the internal heat generation is relatively high and compounded with aggressive external environment [1].

Product

The product in analysis is an automotive electronic product that operates multiple applications in the vehicle. Catering to all these demands require high current flow on board. The product consists of a plastic enclosure that houses PCB and high current capable electronic components. It consists of multiple inputs and output pins to support a variety of applications. The high current is routed out in multiple copper layers. The



International NAFEMS Conference on Engineering Analysis, Modeling, Simulation and 3D-Printing (NAFEMS-3D) – 2016

Full paper

cooper layers, due to the constraint in their size, experience high current density that leads to higher Joule heating. Apart from this, there are several heat dissipating components on board. As a result, components are expected to be at higher temperature.

Electrical-thermal simulation

Electrical-Thermal simulation helps to (i) visualize the thermal field, (ii) identify bottlenecks to current flow, and (iii) identify hot spots in order to optimize the electronic layout for reducing the Joule heating. In this study, Electrical-Thermal simulation is carried out in Adam Research's Thermal Risk Management tool. The tool is used to calculate temperature of components and PCB due to electrical current flow in copper tracks and component heat dissipation.

Simulation model

The model consists of lumped components with their respective power dissipation, thermal vias in PCB underneath the heat dissipating components, PCB base material (FR4), copper layers with discrete tracks for current flow and heat conduction, and electrical nets for current flow among copper layers, input-output pins and components. The effect of enclosure is manifested in the overall heat transfer coefficient that is applied on PCB and components as boundary condition. Overall heat transfer coefficient is derived from a system-level conjugate heat transfer model accounting for convection and radiation for the entire product. Electrical current (I) is assigned to input and out pins. The model allows the current to flow in the entire circuit depending upon connectivity and routing between input and output pins. Ambient temperature is applied to PCB and components as boundary condition.

Validation of Simulation

In order to assess the thermal risk and enhance the life time of the product by removing thermal bottlenecks, temperature of components, PCB and plastic housing is compared with their limits [2]. Since the life time of an electronic product is reduced by half for every 10 °C increase in temperature, it is necessary to have safe operating temperature for components.

Life time and operating temperature of component are related by

$$t = e^{c/T}$$
(3)

Where,

t: life time, hrc: constantT: operating temperature (junction or ambient) of components, K

For validating the simulation results, measurement at board- and component-level is carried out in the lab via IR thermal imaging and thermo-couple measurements for thermal field and component temperature respectively. Simulation and measurement results are found to be within \pm 3%. Table 1 shows the temperature of few operating components that were measured and their predicted temperature in simulation.

1		
Reference Designator	Temperature rise	Temperature rise
	in testing ($^{\circ}$ C)	in simulation (°C)
C1	55.3	57.3
C2	51.2	53.0
C3	56.6	59.3
C4	49.0	53.9
C5	56.0	61.5
C6	50.0	51.7
C7	62.7	69.7
C8	48.5	56.1

Table 1: Comparison of simulation and measurement results

Base Model

Once the simulation model is validated with the lab measurement, a full blown model is simulated with complete loading, where PCB experience maximum current and power dissipation of the components. Copper layer thickness in the base model is considered as below:

	2
Cu Layers	Thickness (Normalized)
Тор	1.0
Inner 1	1.0
Inner 2	1.0
Inner 3	1.0
Inner 4	1.0
Bottom	1.0

Table 2: PCB copper layer thickness in base model

The maximum temperature rise (ΔT) on the board is observed at 88.8 °C. This temperature is observed on the top side of the PCB. The total joule heating is calculated as 13.03 W.



International NAFEMS Conference on Engineering Analysis, Modeling, Simulation and 3D-Printing (NAFEMS-3D) – 2016

Full paper



Fig. 1: Temperature rise on the top side of PCB for Base design



Fig. 2: Temperature rise on the bottom side of PCB for Base design

Design Modification 1

Since the Joule heating is quite high (i.e. 13 W) and contributes to heating the PCB and components, modifications are done on copper tracks to reduce it. As the first step of reducing Joule heating, modifications are done to increase the cross section area of the copper track by increasing the copper layer thickness. The copper layer thickness is considered as below:

Cu Layers	Thickness (normalized)
Тор	2.0
Inner 1	2.0
Inner 2	2.0
Inner 3	2.0
Inner 4	2.0
Bottom	2.0

Table 3: PCB copper layer thickness in design modification 1

The maximum temperature rise on board in this case is observed to be 59.8 $^{\circ}$ C. Joule heating reduces from 13.03 W to 6.81 W. With the increase in copper layer thickness by twice, the cross section area is increased to double. This reduces the joule heating by half.



Fig. 3: Temperature rise on the top side of PCB for Design modification 1



r

Full paper

Design Modification 2

With the increase in Copper layer thickness, the cross section area increases which is an effective way of reducing the Joule heating and maximum temperature on the PCB. In the next design modification, PCB with maximum copper layer thickness available for prototyping is chosen. The copper layer thickness used is mentioned in below table.

Cable 4: PCB copper layer thickness	and joule	heating	in	corresponding	layers	for
design	modificat	ion 2				

Layer	Thickness (normalized)	Joule heating (W)
Тор	1.6	4.76
Inner 1	1.0	0.06
Inner 2	3.0	0.44
Inner 3	3.0	0.31
Inner 4	1.0	0.06
Bottom	1.6	2.44

In design modification 2, maximum temperature rise on PCB is observed as 62.5 $^{\circ}$ C. Total Joule heating is calculated to be 8.23 W.



Fig. 4: Temperature rise on the top side of PCB for Design modification 2

Design Modification 3

Once the PCB with maximum copper layer thickness is utilized, routing is done for increasing the current carrying tracks in fourth inner layer. This leads to distribution of joule heating to inner layer. Maximum PCB temperature on board reduces by 7 K only due to distribution of current to inner layer.

Layer	Thickness (normalized)	Joule heating (W)
Тор	1.6	2.86
Inner 1	1.0	0.07
Inner 2	3.0	0.43
Inner 3	3.0	0.34
Inner 4	1.0	0.48
Bottom	1.6	1.89

 Table 5: PCB copper layer thickness and joule heating in corresponding layers for design modification 3



Fig. 5: Temperature on the top side of PCB for Design modification 3

In this design, maximum temperature rise on PCB is 55.8 $^{\circ}$ C. Total Joule heating in inner layer 4 increases from 0.06 W to 0.48 W.



Full paper

Design Modification 4

After utilizing the inner layers for carrying current, the tracks with maximum current density are widen to increase the cross section. This reduces the joule heating and hence reduces the temperature on PCB.

Table 6: PCB	copper layer	thickness	and jould	e heating	in	corresponding	layers	for
		design	modifica	tion 4				

Layer	Thickness (normalized)	Joule heating (W)
Тор	1.6	2.35
Inner 1	1.0	0.05
Inner 2	3.0	0.38
Inner 3	3.0	0.28
Inner 4	1.0	0.46
Bottom	1.6	2.08

In this case, the maximum temperature rise on PCB is observed to be 53.3 $^{\circ}$ C. Maximum current density is reduced from 140 A/mm² to 120 A/mm² in top layer and from 73 A/mm² to 62 A/mm² in inner layer 4.



Fig. 6: Temperature rise on the top side of PCB for Design modification 4

Conclusion

Reduction in temperature of components and PCB is an important design goal to increase the lifetime of electronic product. To achieve the safe operating temperature on a high current density board, joule heating needs to be minimized. Reduction in joule heating is obtained through optimization of track geometry as exhibited in design modification 1, 2 and 4. To further reduce the maximum temperature of component and PCB, inner layers are utilized to carry the current as in design modification 3.

Overall maximum temperature rise of PCB reduces from 88 °C to 53 °C, which enhances the lifetime of the electronics. This simulation also helps in identifying hot spots at early stage of development and provide measures to mitigate them.

Design	Description	Max. temperature rise of PCB, °C			
Base model	Nominal copper layer thickness $= 1$	88			
Design modification 1	Nominal copper layer thickness $= 2$	59			
Design modification 2	PCB with maximum copper layer	62			
	thickness available for testing				
Design modification 3	Routing to inner copper layer	55			
Design modification 4	Widening of copper tracks on PCB	53			

Table 7: Summary of various design modification studied

References

- 1. [1] Ritwik Alok Pattnayak, Laxmidhar Biswal, "Thermal design and analysis for high power automotive electronic product", The International Conference for Engineering Analysis, Modelling & Simulation Community, NAFEMS World Congress 2015, San Diego, California 2015.
- 2. [2] Nitesh Kumar Sardana, Ritwik Alok Pattnayak, Susyamala Pavan Kumar Busam, Chandan Kumar Ghosh, Laxmidhar Biswal, "Thermal Analysis of a Battery in an Electronic Device for an Outdoor Application", 2016 International Conference on Electronics Packaging